

## 3.6. 基礎の設計

地盤調査方法  
サソビ・インク

地業	:	べた基礎
建物総重量	$\Sigma W$	490.8 (kN)
1階床重量	W1	35.0 (kN)
地盤支持力	$f_e$	20.0 (kN/m <sup>2</sup> )
基礎版面積	A	77.85 (m <sup>2</sup> )
基礎立上り部重量	Wt	88.4 (kN)
スラブ重量	Ws	280.3 (kN)
積載荷重	WL	101.2 (kN)
底版厚	t	15.0 (cm)
かぶり厚	dt	6.5 (cm)
安全率	n	1.1

## 3.6.1. 地盤支持力の検討

$$f_e = 20.00 \text{ (kN/m}^2\text{)}$$

支持力 算定用分布荷重

$$\begin{aligned} \omega_0 &= n \times (\Sigma w + W1 + Wt + Ws + WL) / A \\ &= 1.1 \times (490.83 + 35.04 + 88.37 + 280.26 + 101.21) / 77.85 \\ &= 14.07 \text{ (kN/m}^2\text{)} \leq 20.0 \text{ OK} \end{aligned}$$

スラブ配筋 算定用分布荷重

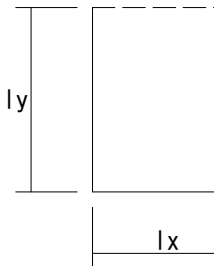
$$\begin{aligned} \omega_1 &= n \times (\Sigma w + Wt) / A \\ &= 1.1 \times (490.83 + 88.37) / 77.85 = 8.18 \text{ (kN/m}^2\text{)} \end{aligned}$$

地中梁配筋 算定用分布荷重

$$\begin{aligned} \omega_2 &= n \times \Sigma w / A \\ &= 1.1 \times 490.83 / 77.85 = 6.94 \text{ (kN/m}^2\text{)} \end{aligned}$$

## 3.6.2. スラブの配筋

FS1 (X6-X13、Y0-Y4)



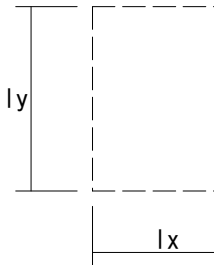
$$l_x = 3.64 \text{ (m)} \quad l_y = 6.37 \text{ (m)} \quad \text{配筋 : D13}$$

$$\omega_1 = 8.18 \text{ (kN/m}^2\text{)}$$

$$\begin{aligned} t &= 15.0 \text{ (cm)} & dt &= 6.5 \text{ (cm)} \\ dx &= t - dt = 8.50 \text{ (cm)} & dy &= t - dt - 1 = 7.50 \text{ (cm)} \\ j_x &= 7/8 \times dx = 7.44 \text{ (cm)} & j_y &= 7/8 \times dy = 6.56 \text{ (cm)} \end{aligned}$$

$$\begin{aligned} \omega_x &= (Ly^4 \times \omega_1) / (Lx^4 + Ly^4) = 7.395 \text{ (kN/m}^2\text{)} \\ M_{x1} &= 1 \times \omega_x \times Lx^2 / 8 = 12.25 \text{ (kN}\cdot\text{m)} & at &= 8.45 \text{ (cm}^2\text{/m)} \\ M_{x2} &= 1 \times \omega_x \times Lx^2 / 18 = 5.44 \text{ (kN}\cdot\text{m)} & at &= 3.75 \text{ (cm}^2\text{/m)} \\ M_{y1} &= 1 \times \omega_1 \times Lx^2 / 12 = 9.04 \text{ (kN}\cdot\text{m)} & at &= 7.06 \text{ (cm}^2\text{/m)} \\ M_{y2} &= 1 \times \omega_1 \times Lx^2 / 36 = 3.01 \text{ (kN}\cdot\text{m)} & at &= 2.35 \text{ (cm}^2\text{/m)} \\ l &= 127 / at_{\text{Max}} = 15.04 \text{ (cm)} \rightarrow \text{D13 @150 両方向} \end{aligned}$$

FS1 (X0-X4、Y3-Y8)



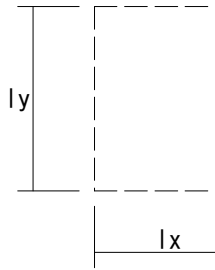
$$l_x = 3.64 \text{ (m)} \quad l_y = 4.55 \text{ (m)} \quad \text{配筋 : D13}$$

$$\omega_1 = 8.18 \text{ (kN/m}^2\text{)}$$

$$\begin{aligned} t &= 15.0 \text{ (cm)} & dt &= 6.5 \text{ (cm)} \\ dx &= t - dt = 8.50 \text{ (cm)} & dy &= t - dt - 1 = 7.50 \text{ (cm)} \\ j_x &= 7/8 \times dx = 7.44 \text{ (cm)} & j_y &= 7/8 \times dy = 6.56 \text{ (cm)} \end{aligned}$$

$$\begin{aligned} \omega_x &= (Ly^4 \times \omega_1) / (Lx^4 + Ly^4) = 5.806 \text{ (kN/m}^2\text{)} \\ M_{x2} &= 1 \times \omega_x \times Lx^2 / 8 = 9.62 \text{ (kN}\cdot\text{m)} & at &= 6.63 \text{ (cm}^2\text{/m)} \\ M_{y2} &= 1 \times \omega_1 \times Lx^2 / 27 = 4.02 \text{ (kN}\cdot\text{m)} & at &= 3.14 \text{ (cm}^2\text{/m)} \\ l &= 127 / at_{\text{Max}} = 19.16 \text{ (cm)} \rightarrow \text{D13 @150 両方向} \end{aligned}$$

## FS2 (X6-X13、Y4-Y6)



$$l_x = 1.82 \text{ (m)}$$

$$\omega_1 = 8.18 \text{ (kN/m}^2\text{)}$$

$$l_y = 6.37 \text{ (m)}$$

配筋 : D10

$$t = 15.0 \text{ (cm)}$$

$$dx = t - dt = 8.50 \text{ (cm)}$$

$$j_x = 7/8 \times dx = 7.44 \text{ (cm)}$$

$$dt = 6.5 \text{ (cm)}$$

$$dy = t - dt - 1 = 7.50 \text{ (cm)}$$

$$j_y = 7/8 \times dy = 6.56 \text{ (cm)}$$

$$\omega_x = (L_y^4 \times \omega_1) / (L_x^4 + L_y^4) = 8.130 \text{ (kN/m}^2\text{)}$$

$$M_{x2} = 1 \times \omega_x \times L_x^2 / 8 = 3.37 \text{ (kN}\cdot\text{m)} \quad at = 2.32 \text{ (cm}^2\text{/m)}$$

$$M_{y2} = 1 \times \omega_1 \times L_x^2 / 27 = 1.00 \text{ (kN}\cdot\text{m)} \quad at = 0.78 \text{ (cm}^2\text{/m)}$$

$$l = 71 / at_{\text{Max}} = 30.59 \text{ (cm)} \rightarrow \text{D10 @300 両方向}$$

※実際は3辺固定だが、安全側のみで0辺固定で設計。  
他の耐圧版のこの大きさ以下であり、同様の符号とする。